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Abstract

We will show how to obtain the two first orders of the expansion of the potential flow induced by a curved vortex line. The expansion is done on the distance r to the line and is performed by using the method of matched asymptotic expansion of singular integral. The order O(r) of this expansion will be given with both its local and global integral parts. This method will also be used to give the inner expansion of the flow induced by a slender vortex with the slenderness ϵ as the expansion parameter and an application will be given for a circular vortex ring with axial core structure variation. Finally we will summarise the derivation of the equation of motion of the central line [Callegari and Ting SIAM J.Appl. Math. 35(1), 1978], give its generalisation at next order and speak about its generalisation to a curved filament with axial variation.

Outline

Velocity and vorticity equations

The induced velocity field of a curved vortex

The curved vortex line The velocity expansion near the curved line The proof : the MAESI Method The curved slender vortex Application to a slender vortex with axial variation

Equation of motion of a curved slender filament

The equation of motion The derivation of the equation of motion

- 1. Equations on curvilinear coordinates
- 2. Expansions and Matching
- 3. The resulting equation of motion
- 4. Core equations : the compatibility conditions

Generalisation, Axial variation

Velocity and vorticity equations

> Domaine of study: Incompressive laminar flows with vorticity and $Re \gg 1$

$$\boxed{ \frac{\partial \mathbf{v}}{\partial t} + \mathbf{v} \nabla \mathbf{v} = -\nabla \frac{p}{\rho} + \nu \Delta \mathbf{v} }$$
$$\nabla \cdot \mathbf{v} = 0$$

The field of Vorticity

$$\boldsymbol{\omega} = \nabla imes \mathbf{v}$$

$$rac{\partial \omega}{\partial t} + \mathbf{v}
abla \omega = \omega
abla \mathbf{v} +
u \Delta \omega$$

Biot and Savart

$$\mathbf{v}(\mathbf{x}) =
abla arphi(\mathbf{x}) + rac{1}{4\pi} \int\!\!\!\int\!\!\!\int rac{\omega(\mathbf{x}') imes (\mathbf{x}-\mathbf{x}')}{|\mathbf{x}-\mathbf{x}'|^3} d\mathbf{x}',$$

Background velocity $abla arphi(\mathbf{x})$ + Induced velocity

The induced velocity field of a curved vortex

The curved vortex line

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Generalisation, Axial variation

- The induced velocity field of a curved vortex

└─ The curved vortex line

The curved vortex line

The curved filament without thickness $\boldsymbol{\omega} = \Gamma \delta_{\mathcal{C}} \mathbf{t}$





- The induced velocity field of a curved vortex

L The curved vortex line

The velocity expansion near the curved line

If $\boldsymbol{\omega} = \boldsymbol{\Gamma} \delta_{\mathcal{C}} \mathbf{t}$ then

$$\mathbf{v}(\mathbf{x}) = \frac{\Gamma}{4\pi} \int_{\mathcal{C}} \frac{\mathbf{t}(a') \times (\mathbf{x} - \mathbf{X}(a'))}{|\mathbf{x} - \mathbf{X}(a')|^3} da'$$
$$\mathbf{v}(r \to 0) = \frac{\Gamma}{4\pi} \mathbf{e}_{\theta} + \frac{\Gamma}{4\pi} K \ln \frac{\mathcal{L}}{r} \mathbf{b} + \mathbf{Q}_f + O(r)$$

- The induced velocity field of a curved vortex

L The curved vortex line

The leading order expansion near the curved line

Dimensionless : length L = O(1/K) velocity Γ/L

$$\mathbf{v}(r o 0, arphi, \mathbf{a}) = rac{1}{2\pi r} \mathbf{e}_{ heta} + rac{K}{4\pi} \cos arphi \mathbf{e}_{ heta} + \mathbf{A} + rac{K}{4\pi} \left[\ln rac{S}{r} - 1
ight] \mathbf{b} + O(r)$$

where

$$\mathbf{A}(a) = \frac{1}{4\pi} \int_{-S/2}^{+S/2} [\frac{\mathbf{t}(a+a^*) \times \mathbf{d}}{|\mathbf{d}|^3} - \frac{K(a)\mathbf{b}(a)}{2|a^*|}] da^*,$$

with $\mathbf{d} = \mathbf{X}(a) - \mathbf{X}(a + a^*)$ Result :

$$\mathcal{L} = S$$

$$\mathbf{Q}_{f} = \frac{\Gamma K}{4\pi} \left(\cos \varphi \mathbf{e}_{\theta} - \mathbf{b} \right) + \Gamma \mathbf{A}$$

The induced velocity field of a curved vortex

L The curved vortex line

The first order expansion near the curved line

Dimensionless : length L = O(1/K) velocity Γ/L

$$\mathbf{v}(r \to 0, \varphi, \mathbf{a}) = \frac{1}{2\pi r} \mathbf{e}_{\theta} + \frac{K}{4\pi} \cos \varphi \mathbf{e}_{\theta} + \mathbf{A} + \frac{K}{4\pi} \left[\ln \frac{S}{r} - 1 \right] \mathbf{b}$$
$$+ r\mathbf{I} + \frac{1}{4\pi} \left(\mathbf{B} - 3\mathbf{C} - \frac{4}{S^2} \mathbf{e}_{\theta} \right) r + O(r^2 \ln r),$$

where 1

$$\mathbf{I} = \frac{3}{16} \frac{K^2}{\pi} \left[\left(\mathbf{e}_r \sin 2\varphi + \mathbf{e}_\theta \cos 2\varphi \right) \left(\ln \frac{S}{r} - \frac{4}{3} \right) \right] \\ + \frac{3}{16} \frac{K^2}{\pi} \left[\frac{1}{2} \mathbf{e}_\theta \cos 2\varphi + \frac{1}{18} \mathbf{e}_\theta \right] \\ + \frac{1}{4\pi} \left(K_\theta \sin \varphi - KT \cos \varphi \right) \left[\ln \frac{S}{r} - 1 \right] \mathbf{t}.$$

¹Y. Fukumoto and T. Miyazaki. "Three dimensional distortions of a vortex filament with axial velocity". In: J. Fluid Mech. 222 (1991), pp. 369–416.

The induced velocity field of a curved vortex

L The curved vortex line

The first order expansion near the curved line

$$\begin{split} \mathbf{A}(a) &= \frac{1}{4\pi} \int_{-S/2}^{+S/2} \left[\frac{\mathbf{t}(a+a^*) \times \mathbf{d}}{|\mathbf{d}|^3} - \frac{K(a)\mathbf{b}(a)}{2|a^*|} \right] da^*, \\ \mathbf{B}(\varphi, a) &= \mathbf{e}_r(\varphi, a) \times \int_{-S/2}^{+S/2} \left[-\frac{\mathbf{t}(a+a^*)}{|\mathbf{d}|^3} - f_b(a, a^*) \right] da^*, \\ \mathbf{C}(\varphi, a) &= \int_{-S/2}^{+S/2} \left[\frac{\mathbf{e}_r(\varphi, a) \cdot \mathbf{d}}{|\mathbf{d}|^5} \left[\mathbf{t}(a+a^*) \times \mathbf{d} \right] - f_c(a, a^*) \right] da^*, \end{split}$$

with $\mathbf{d} = \mathbf{X}(a) - \mathbf{X}(a + a^*)$ and²

$$\begin{split} f_b(a,a^*) &= -\frac{1}{|a^*|^3} [\mathbf{t}(a) + \mathcal{K}(a)\mathbf{n}(a)a^*] \\ &\quad -\frac{1}{|a^*|^3} [\frac{a^{*2}}{2} [\mathcal{K}_a(a)\mathbf{n}(a) + \mathcal{K}(a)\mathcal{T}(a)\mathbf{b}(a) - \frac{3}{4}\mathcal{K}^2(a)\mathbf{t}(a)]] \\ f_c(a,a^*) &= -\frac{\mathcal{K}^2(a)\mathbf{b}(a)\cos(\varphi)}{4|a^*|}. \end{split}$$

²D. Margerit and J-P Brancher. "Asymptotic expansions of the Biot-Savart law for a slender vortex with core variation". In: *Journal of Engineering Mathematics* 40.3 (2001), pp. 297–313.

The induced velocity field of a curved vortex

L The curved vortex line

The proof : the MAESI Method

MAESI = Matched Asymptotic Expansion of Singular Integral³

1. Change of variable $a^* = a' - a$ is done :

$$\begin{split} \mathbf{v}(r,\varphi,\mathbf{a}) &= \frac{1}{4\pi} \int_{\mathcal{C}} \frac{\mathbf{t}(\mathbf{a}') \times (\mathbf{x} - \mathbf{X}(\mathbf{a}'))}{|\mathbf{x} - \mathbf{X}(\mathbf{a}')|^3} d\mathbf{a}' \\ &= \frac{1}{4\pi} \int_{-S/2}^{+S/2} \mathbf{K}(r,\varphi,\mathbf{a},\mathbf{a}^*) d\mathbf{a}^*, \end{split}$$

2. Small intermediate parameter η with $r \ll \eta \ll 1$

$$\mathsf{v}(\mathsf{r},arphi,\mathsf{a})=\mathsf{E}\mathsf{x}+\mathsf{I}\mathsf{n}$$

$$\begin{aligned} \mathbf{Ex} &= \frac{1}{4\pi} \int_{-S/2}^{-\eta} \mathbf{K} da^* + \frac{1}{4\pi} \int_{\eta}^{+S/2} \mathbf{K} da^* \\ \mathbf{In} &= \frac{1}{4\pi} \int_{-\eta}^{\eta} \mathbf{K} da^* \end{aligned}$$

³C. François. Les méthodes de perturbation en mécanique. 98-104. Paris: ENSTA, 1981.

The induced velocity field of a curved vortex

L The curved vortex line

The proof : the MAESI Method

3. Stretched variable $\bar{a} = a^*/r$ introduced

$$\ln = \frac{1}{4\pi} r \int_{-\eta/r}^{\eta/r} \tilde{\mathsf{K}} d\bar{\mathsf{a}}$$

$$ilde{\mathsf{K}}(r,arphi, \mathsf{a}, ar{\mathsf{a}}) = \mathsf{K}(r, arphi, \mathsf{a}, rar{\mathsf{a}})$$

- 4. Outer Part : expansion with r of Ex
 - expansion of K with r and integrate
 - expansion with $\eta \ll 1$

Example :

$$\int_{\eta}^{+S/2} \frac{\mathbf{t}(a+a^*) \times \mathbf{d}}{|\mathbf{d}|^3} da^* = \int_{\eta}^{+S/2} \frac{\mathcal{K}(a)\mathbf{b}(a)}{2|a^*|} da^* + \int_{\eta}^{+S/2} [\frac{\mathbf{t}(a+a^*) \times \mathbf{d}}{|\mathbf{d}|^3} - \frac{\mathcal{K}(a)\mathbf{b}(a)}{2|a^*|}] da^*$$

because

$$\mathbf{t}(\mathbf{a}+\mathbf{a}^*)\times\mathbf{d}/|\mathbf{d}|^3=K(\mathbf{a})\mathbf{b}(\mathbf{a})/2|\mathbf{a}^*|+O(1)$$

The induced velocity field of a curved vortex

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The proof : the MAESI Method

- 5. Inner part : expansion with r of In
 - expansion of $\tilde{\mathbf{K}}$ with r and integrate
 - expansion of **In** with $\eta/r \gg 1$
- 6. Addition of Ex and In :



 η disappears

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The curved slender vortex

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The curved slender vortex

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Generalisation, Axial variation

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The flow induced by a curved slender vortex

$$\mathbf{v}(\mathbf{x}) = rac{1}{4\pi} \int \int \int rac{\omega(\mathbf{x}') imes (\mathbf{x} - \mathbf{x}')}{|\mathbf{x} - \mathbf{x}'|^3} d\mathbf{x}',$$

Dimensionless : length L = O(1/K) velocity Γ/L

• Outer limit : $\epsilon \to 0$ with r fixed: $\mathbf{v}^{out} = \mathbf{v}^{out(0)} + \epsilon \mathbf{v}^{out(1)} + O(\epsilon^2)$

lnner limit : $\epsilon \to 0$ with $\bar{r} = r/\epsilon$ fixed: $\mathbf{v}^{inn} = \epsilon^{-1} \mathbf{v}^{inn(0)} + \mathbf{v}^{inn(1)} + O(\epsilon)$

$$\mathbf{v}(r,\varphi,\mathbf{s},t,\epsilon) = \\ \frac{1}{4\pi} \int \int \int \frac{\epsilon^2 \boldsymbol{\omega}(\bar{r}',\varphi',\mathbf{a}',\epsilon) \times \left[\mathbf{X} + r\mathbf{e}_r - (\mathbf{X}' + \epsilon \bar{r}'\mathbf{e}'_r)\right]}{\left|\mathbf{X} + r\mathbf{e}_r - (\mathbf{X}' + \epsilon \bar{r}'\mathbf{e}'_r)\right|^3} h'_3 \bar{r}' d\bar{r}' d\varphi' d\mathbf{a}',$$

where $h'_3 = (1 - K(a')\epsilon \bar{r}' \cos(\varphi'))$. Problem : Velocity induced by $\omega(\mathbf{x}) = \omega(\bar{r}, \varphi, \mathbf{a}, \epsilon) = \epsilon^{-2}\omega^{(0)}(\bar{r}, \varphi, \mathbf{a})$

- The induced velocity field of a curved vortex
 - L The curved slender vortex

The flow induced by a curved slender vortex

▶
$$\mathbf{v}^{out(0)}$$
 : line vortex, $\mathbf{v}^{out(1)} \neq 0$

• MAESI⁴ method in ϵ :

$${f v}^{inn(0)}=-rac{1}{2\pi}\int\int {f g}ar r' dar r' dar \gamma'$$

where

$$\mathbf{g} = \omega^{(0)}(\bar{r}', \varphi', \mathbf{a}) \times \left[\bar{r}' \mathbf{e}_r(\varphi', \mathbf{a}) - \bar{r} \mathbf{e}_r(\varphi, \mathbf{a})\right] / k^2$$

$$k^2 = \bar{r}^2 + \bar{r}'^2 - 2\bar{r}\bar{r}' \cos(\varphi - \varphi')$$

⁴Margerit and Brancher, "Asymptotic expansions of the Biot-Savart law for a slender vortex with core variation".

 \sqsubseteq The induced velocity field of a curved vortex

L_The curved slender vortex

The flow induced by a curved slender vortex

$$\mathbf{v}^{inn(1)} = \mathbf{A} + \frac{K}{4\pi} [\ln \frac{S}{\epsilon} - 1] \mathbf{b}$$

$$- \frac{1}{4\pi} \iint \omega_a^{(0)}(\bar{r}', \varphi', a) \times \mathbf{t}(a) \ln \frac{1}{k^2} \bar{r}' d\bar{r}' d\varphi'$$

$$- \frac{K(a)}{8\pi} \iint \omega^{(0)}(\bar{r}', \varphi', a) \times \mathbf{n}(a) \ln \frac{1}{k^2} \bar{r}' d\bar{r}' d\varphi'$$

$$- \frac{K(a)\bar{r}\cos(\varphi)}{4\pi} \iint \mathbf{g}\bar{r}' d\bar{r}' d\varphi' + \frac{K(a)}{4\pi} \iint \mathbf{g}\cos\varphi' \bar{r}'^2 d\bar{r}' d\varphi',$$

$$- \frac{T(a)\bar{r}}{2\pi} \iint \frac{\omega^{(0)}(\bar{r}', \varphi', a) \times \mathbf{t}(a)}{k^2} \sin(\varphi - \varphi') \bar{r}'^2 d\bar{r}' d\varphi'$$

where

$$\mathbf{g} = \omega^{(0)}(\bar{r}', \varphi', \mathbf{a}) \times \left[\bar{r}' \mathbf{e}_r(\varphi', \mathbf{a}) - \bar{r} \mathbf{e}_r(\varphi, \mathbf{a})\right] / k^2$$

$$k^2 = \bar{r}^2 + \bar{r}'^2 - 2\bar{r}\bar{r}' \cos(\varphi - \varphi')$$

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Application to a slender vortex with axial variation

Chosen vorticity⁵

$$\omega = \frac{1}{\epsilon^2} \left[\frac{1}{\pi \bar{r}_0^2(a)} \mathbf{t} + \epsilon \frac{\bar{r}_0'(a)}{\pi \bar{r}_0^3(a)} \frac{\bar{r}}{h_3} \mathbf{e}_r + \frac{g(a,\bar{r})}{h_3} \mathbf{e}_\theta \right] H\left(1 - \frac{\bar{r}}{\bar{r}_0(a)}\right)$$



 ${
m div}\omega=0$ and $\omega\cdot {f N}=0$ on $ar r=ar r_0(a)$

• Decomposition
$$\mathbf{v} = \mathbf{v}(\bar{r} = 0, a) + \mathbf{V}$$

 $^{^5}$ Margerit and Brancher, "Asymptotic expansions of the Biot-Savart law for a slender vortex with core variation".

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Application to a slender vortex with axial variation

lnduced velocity : $(g(a, \overline{r}) = 0)$

$$\begin{split} \mathbf{V}^{inn(0)} &=& \frac{\bar{r}}{2\pi\bar{r}_0^2} \mathbf{e}_\theta \text{ if } \bar{r} < \bar{r}_0(s) \\ &=& \frac{1}{2\pi\bar{r}} \mathbf{e}_\theta \text{ if } \bar{r} > \bar{r}_0(s), \end{split}$$

$$\mathbf{V}^{inn(1)} = -\left(\frac{\bar{r}}{\bar{r}_0}\right)^2 \frac{K}{16\pi} \left[3\sin\varphi\mathbf{e}_r + \cos\varphi\mathbf{e}_\theta\right] \quad \text{if } \bar{r} < \bar{r}_0(s)$$
$$= -\frac{K}{16\pi} \left(\left[-\left(\frac{\bar{r}_0}{\bar{r}}\right)^2 + 4 + 4\ln\frac{\bar{r}}{\bar{r}_0}\right]\sin\varphi\mathbf{e}_r + \left[\left(\frac{\bar{r}_0}{\bar{r}}\right)^2 + 4\ln\frac{\bar{r}}{\bar{r}_0}\right]\cos\varphi\mathbf{e}_\theta\right) \text{ if } \bar{r} > \bar{r}_0(s)$$

and

$$\mathbf{v}(\bar{r}=0,a) = \mathbf{A} + rac{K\mathbf{b}}{4\pi} \left[\ln rac{S}{(\epsilon \bar{r}_0)}
ight]$$

Equation of motion of a curved slender filament

- The equation of motion

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The curved slender filament



 $\mathbf{v} = \dot{\mathbf{X}}(s, t) + \mathbf{V}$ $\mathbf{V} = u\mathbf{e}_r + v\mathbf{e}_{\theta} + w\mathbf{t}$

Dimensionless :

length $L = O(1/K) \gg I = O(\delta)$, $I/L = \epsilon$, velocity Γ/L

$$Re = rac{\Gamma}{
u} = rac{1}{lpha^2 \epsilon^2} \gg 1$$
 $Sw = rac{\Gamma\delta}{M} = rac{\epsilon}{M} = rac{1}{m} + O(\epsilon)$

Equation of motion of a curved slender filament

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Equation of Callegari and Ting⁶

$$\dot{\mathbf{X}}(s,t)= \mathbf{Q}+rac{\mathcal{K}(s,t)}{4\pi}\left[\ln(S/\epsilon)-1+\mathcal{C}_{v}(t)+\mathcal{C}_{w}(t)
ight]\mathbf{b}(s,t)$$

with
$$\mathbf{Q} = \mathbf{A}(s,t) - [\mathbf{A}(s,t) \cdot \mathbf{t}(s,t)] \mathbf{t}(s,t)$$

 $\mathbf{A}(s,t) = \frac{1}{4\pi} \int_{-\pi}^{+\pi} ds' \ \sigma' \left[\frac{\mathbf{t}(s+s',t) \times \mathbf{d}}{|\mathbf{d}|^3} - \frac{\mathbf{K}(s,t)\mathbf{b}(s,t)}{2|\lambda(s,s',t)|} \right]$
 $\mathbf{d} = \mathbf{X}(s,t) - \mathbf{X}(s+s',t)$

⁶A.J. Callegari and L. Ting. "Motion of a curved vortex filament with decaying vortical core and axial velocity". In: *SIAM J. Appl. Math.* 35.1 (1978), pp. 148–175.

Equation of motion of a curved slender filament

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Cut-off equations

$$\partial \mathbf{X} / \partial t = \frac{1}{4\pi} \int_{l} \sigma(s', t) \frac{\mathbf{t}(s', t) \times (\mathbf{X}(s, t) - \mathbf{X}(s', t))}{|\mathbf{X}(s, t) - \mathbf{X}(s', t)|^3} ds'$$

where $I = [0, 2\pi[\setminus [s - s_c, s + s_c]$ s_c : cut-off length Singular Integral for the small parameter s_c MAESI + Comparison⁷

$$s_c(s,t) = \epsilon \exp\left(1 - \ln 2 - C_v(t) - C_w(t)\right) / \sigma(s,t)$$

Regularization methods

⁷D. Margerit. "Mouvement et dynamique des filaments et des anneaux tourbillons de faible épaisseur". PhD thesis. Institut National Polytechnique de Lorraine, 1997.

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The equation of motion

The derivation of the equation of motion

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Generalisation, Axial variation

Equation of motion of a curved slender filament

L The derivation of the equation of motion

1. Equations on curvilinear coordinates (r, φ, s)

$$\mathbf{v}(r,\varphi,s,t,\epsilon) = \dot{\mathbf{X}}(s,t,\epsilon) + \mathbf{V}(r,\varphi,s,t,\epsilon)$$
$$\mathbf{V} = u\mathbf{e}_r + v\mathbf{e}_\theta + w\mathbf{t}$$

- Biot and Savart in local coordinates
- Continuity in local coordinates

$$(urh_3)_r + (h_3v)_{\varphi} + rw_s - Trw_{\varphi} = -r\dot{\mathbf{X}}_s \cdot \mathbf{t}$$

where $h_3 = \sigma \left(1 - rK(s)\cos(\varphi)\right)$ and $\sigma = |\mathbf{X}_s|$

Navier-Stokes in local coordinates

$$\mathbf{a} = -\nabla p + \nu \Delta \mathbf{V} + \frac{\nu}{h_3} \left(\frac{1}{h_3} \dot{\mathbf{X}}_s\right)_s$$
$$\mathbf{a} = \left(\frac{\partial \mathbf{V}}{\partial t}\right)_{r,\varphi,s} + (\mathbf{V} - r\dot{\mathbf{e}}_r) \cdot \nabla \mathbf{V} + \frac{\dot{\mathbf{X}}_s}{h_3} (w - r\dot{\mathbf{e}}_r \cdot \mathbf{t})$$
$$\left(\frac{\partial \mathbf{V}}{\partial t}\right)_{r,\varphi,s} = \frac{\partial u}{\partial t} \mathbf{e}_r + u\dot{\mathbf{e}}_r + ...$$

Equation of motion of a curved slender filament

- The derivation of the equation of motion

2. Expansions and Matching

$${f X} = {f X}^{(0)}(s,t) + \epsilon {f X}^{(1)}(s,t) + ...$$

• Outer limit: $\epsilon \rightarrow 0$ with *r* fixed:

$$\mathbf{v}^{out} = \mathbf{v}^{out(0)} + \epsilon \mathbf{v}^{out(1)} + O(\epsilon^2)$$

Expansion in the Biot Savart law
Matching law: expansion at r = 0 and replace r = r
e is Boundary Conditions at r
is a Boundary Condition

Equation of motion of a curved slender filament

L- The derivation of the equation of motion

2. Expansions and Matching



Figure: Relative velocity field : horizontal axis is the normal and vertical axis is the binormal

Equation of motion of a curved slender filament

L The derivation of the equation of motion

3. The resulting equation of motion

Equation of motion for $\mathbf{X}^{(0)}$

$$\dot{\mathbf{X}}^{(0)}(s,t) = \mathbf{Q} + rac{\mathcal{K}(s,t)}{4\pi} \left[-\ln\epsilon + \ln(S) - 1 + \mathcal{C}_{v}(t) + \mathcal{C}_{w}(t)
ight] \mathbf{b}(s,t)$$

Equation of motion for $\mathbf{X}^{(1)}$: Fukumoto and Miyazaki⁸ + correcting terms

$$\dot{\mathbf{X}}^{(1)} = \mathbf{E}_1 + c_n \mathbf{n}(s, t) + \left\{ C_1^* + \frac{m}{4\pi} \mathcal{K} T\left[\ln \epsilon + \frac{5}{6} - \ln S \right] \right\} \mathbf{b}(s, t)$$

$$c_n = C_2^* - rac{1}{8\pi} \mathcal{K}^{(1)}(s,t) + rac{1}{4\pi} \mathcal{K}^{(1)}(s,t) \ln \epsilon - rac{m}{4\pi} \mathcal{K}_s \left[3 \ln \epsilon + 3 + rac{5}{6} - 3 \ln S
ight]$$

⁸Fukumoto and Miyazaki, "Three dimensional distortions of a vortex filament with axial velocity".

Equation of motion of a curved slender filament

The derivation of the equation of motion

4. Core equations : the compatibility condition

Compatibility conditions for the symmetrical leading order v⁽⁰⁾ and w⁽⁰⁾ do not depend on s

Non-axisymmetric first order only depend on leading order

Temporal equations for the symmetrical leading order : closed vortex⁹

$$\frac{\partial v^{(0)}}{\partial t} - \alpha^2 \left(\left[\frac{1}{\bar{r}} (\bar{r} v^{(0)})_{\bar{r}} \right]_{\bar{r}} - \frac{v^{(0)}}{\bar{r}^2} \right) = \frac{1}{2} \left(\bar{r} v^{(0)} \right)_{\bar{r}} \frac{\dot{S}^{(0)}}{S^{(0)}}$$
$$\frac{\partial w^{(0)}}{\partial t} - \alpha^2 \frac{1}{\bar{r}} \left[\bar{r} w^{(0)}_{\bar{r}} \right]_{\bar{r}} = \frac{1}{2} \bar{r}^3 \left(\frac{w^{(0)}}{\bar{r}^2} \right)_{\bar{r}} \frac{\dot{S}^{(0)}}{S^{(0)}}$$

S(t) is the length of the closed filament

⁹Callegari and Ting, "Motion of a curved vortex filament with decaying vortical core and axial velocity".

Equation of motion of a curved slender filament

The derivation of the equation of motion

4. Core equations : the compatibility condition

• Compatibility conditions for the axisymmetric part $v_c^{(1)}$, $w_c^{(1)}$ of first order $v_c^{(1)}$ does not dependent on s and $w_c^{(1)}$ such that :

$$rac{\partial w_c^{(1)}(ar r,s,t)}{\partial s} = - \dot \sigma^{(0)} + rac{\dot S^{(0)}}{S^{(0)}} \sigma^{(0)}$$

Non-axisymmetric second order only depend on leading order Temporal equations for the axisymmetric part first order : closed vortex $^{10}\,$

$$\frac{\partial v_c^{(1)}}{\partial t} - \alpha^2 \left(\left[\frac{1}{\bar{r}} (\bar{r} v_c^{(1)})_{\bar{r}} \right]_{\bar{r}} - \frac{v_c^{(1)}}{\bar{r}^2} \right) - \frac{1}{2} \left(\bar{r} v_c^{(1)} \right)_{\bar{r}} \frac{\dot{S}^{(0)}}{S^{(0)}} = c_1^{(1)}(\bar{r}, t)$$
$$\frac{\partial w_c^{(1)}}{\partial t} - \alpha^2 \frac{1}{\bar{r}} \left[\bar{r} w_c_{\bar{r}}^{(1)} \right]_{\bar{r}} - \frac{1}{2} \bar{r}^3 \left(\frac{w_c^{(1)}}{\bar{r}^2} \right)_{\bar{r}} \frac{\dot{S}^{(0)}}{S^{(0)}} = c_2^{(1)}(\bar{r}, t)$$

¹⁰D. Margerit. "The complete first order expansion of a slender vortex ring". In: *IUTAM Symposium on Dynamics of Slender Vortices*. Ed. by E. Krause and K. Gersten. Aachen: Kluwer academic publishers, 31 Aug.-3 Sep. 1997, pp. 45–54.

Generalisation, Axial variation

Outline

Velocity and vorticity equations

The induced velocity field of a curved vortex

The curved vortex line The velocity expansion near the curved line The proof : the MAESI Method The curved slender vortex Application to a slender vortex with axial variation

Equation of motion of a curved slender filament

The equation of motion The derivation of the equation of motion

- 1. Equations on curvilinear coordinate
- 2. Expansions and Matching
- 3. The resulting equation of motion
- 4. Core equations : the compatibility conditions

Generalisation, Axial variation

Generalisation, Axial variation

Generalisation, Axial variation

- Short time t/ϵ^2 :
 - Initial velocity of the vortex filament ≠ One-time analysis Performed in 2-d : Ting and Tung Phy. Fluid¹¹
 - leading order not axisymmetric
 - leading order axisymmetric and short waves $\bar{s} = s/\epsilon$: Widnall instability
- Weak Axial variation One-time analysis : $\xi = s\epsilon$ Klein and Ting¹²

 Axial variation One-time analysis : Klein and Ting, Appl. Math. Lett¹³ Temporal equations for a leading order compatible that depends on s

¹¹L. Ting and C. Tung. "Motion and Decay of a Vortex in a Nonuniform Stream". In: Motion and Decay of a Vortex in a Nonuniform Stream. The Physics of Fluids 8.6 (1965), pp. 1039–1051.

 ¹²L. Ting and R. Klein. Viscous Vortical Flows (Monograph). 181-185. Springer: Lecture Notes in Physics, 1991.
 ¹³R. Klein and L. Ting, "Vortex filaments with axial core structure variation". In: Appl.Math.Lett. 5 (1992).

²³R. Klein and L. Ting. "Vortex filaments with axial core structure variation". In: *Appl.Math.Lett.* 5 (1992) pp. 99–103.

Generalisation, Axial variation

- Ad-hoc studies (toy models) :
 - Lundgren Ashurst : Area-varying waves JFM¹⁴
 - Marshall : Curved vortices with variable core area JFM¹⁵
 - Leonard : Nonlocal theory of area-varying waves Phys.Fluids¹⁶

¹⁴T.S. Lundgren and W.T. Ashurts. "Area-varying waves on curved vortex tubes with application to vortex breakdown". In: Area-varying waves on curved vortex tubes with application to vortex breakdown. J. Fluid Mech. 200 (1989), pp. 283–307.

¹⁵ J.S. Marshall. "A general theory of curved vortices with circular cross-section and variable core area". In: A general theory of curved vortices with circular cross-section and variable core area. J. Fluid Mech. 229 (1991), pp. 311–338.

¹⁶A. Leonard. "Nonlocal theory of area-varying waves on axisymmetric vortex tubes". In: Nonlocal theory of area-varying waves on axisymmetric vortex tubes. Phys.Fluids A 6.2 (1994), pp. 765–777.

Symmetrical axial variations

Short time
$$\tau = t/\epsilon$$
 :

leading order axisymmetric and axial variation The compatibility conditions become

$$(\bar{\tau}u_c^{(1)})_{\bar{\tau}} + \frac{\bar{\tau}}{\sigma^{(0)}}w_s^{(0)} = 0$$
$$\frac{\partial v^{(0)}}{\partial \tau} + \frac{\left(\bar{\tau}v^{(0)}\right)_{\bar{\tau}}}{\bar{\tau}}u_c^{(1)} + \frac{w^{(0)}}{\sigma^{(0)}}v_s^{(0)} = 0$$
$$\frac{\partial w^{(0)}}{\partial \tau} + w_{\bar{\tau}}^{(0)}u_c^{(1)} + \frac{p_s^{(0)}}{\sigma^{(0)}} + \frac{w^{(0)}}{\sigma^{(0)}}w_s^{(0)} = 0$$
$$p^{(0)} = -\int_{\bar{\tau}}^{\infty}\frac{v^{(0)^2}}{\bar{\tau}}d\bar{\tau}$$

"Long wave scaling" (Shallow water)

$$u_c^{(1)} = -\frac{1}{\sigma^{(0)}\bar{r}}\psi_s$$
$$w^{(0)} = \frac{1}{\bar{r}}\psi_{\bar{r}}$$

Symmetrical axial variations

$$\begin{array}{rcl}
 \Gamma &=& \overline{r}v^{(0)} \\
 y &=& \overline{r}^2
 \end{array}$$

$$\frac{\partial\Gamma}{\partial\tau} - \frac{2}{\sigma^{(0)}}\psi_s\Gamma_y + \frac{2}{\sigma^{(0)}}\psi_y\Gamma_s = 0$$
$$D^2\frac{\partial\psi}{\partial\tau} + \frac{2}{\sigma^{(0)}}\psi_yD^2\psi_s + \frac{2}{y^2\sigma^{(0)}}\Gamma\Gamma_s - \frac{2}{\sigma^{(0)}}y\psi_s\left[y^{-1}D^2\psi\right] = 0$$
$$D^2\psi = rw_r^{(0)} = 4y\psi_{yy}$$
(1)

See Leibovich¹⁷ length $L = O(1/K) \gg I = O(\delta)$, $I/L = \epsilon$, velocity Γ/L

¹⁷S. Leibovich. "Weakly non-linear waves in rotating fluids". In: Weakly non-linear waves in rotating fluids. J. Fluid Mech. 42 (1970), pp. 803–822.

Symmetrical axial variations

length $L = O(1/K) \gg I = O(\delta)$, $I/L = \epsilon$, velocity Γ/L



Similar vortex

S(t) length of the closed filament

$$\begin{aligned} v^{(0)} &= \frac{1}{2\pi\bar{r}} \left[1 - e^{-\left(\bar{r}/\bar{\delta}\right)^2} \right] \\ w^{(0)} &= \frac{m_0}{\pi\bar{\delta}^2} \left(\frac{S_0}{S} \right) e^{-\left(\bar{r}/\bar{\delta}\right)^2} \\ \bar{\delta}^2 &= \frac{S_0}{S} \left(1 + 4\alpha^2 \int_0^t \frac{S(t^*)}{S_0} dt^* \right) \end{aligned}$$

$$egin{split} \mathcal{C}_{v}(t) &= \left(1+\gamma-\ln 2
ight)/2 - \ln ar{\delta} \ \mathcal{C}_{w}(t) &= -2\left(rac{S_{0}}{S}
ight)^{4}\left(m_{0}/ar{\delta}
ight)^{2} \end{split}$$

Similar vortex



Leading order compatibility conditions with symmetrical axial variation

$$(\bar{\tau}u_c^{(1)})_{\bar{\tau}} + \frac{\bar{\tau}}{\sigma^{(0)}}w_s^{(0)} = 0$$
$$\frac{(\bar{\tau}v^{(0)})_{\bar{\tau}}}{\bar{\tau}}u_c^{(1)} + \frac{w^{(0)}}{\sigma^{(0)}}v_s^{(0)} = 0$$
$$w_{\bar{\tau}}^{(0)}u_c^{(1)} + \frac{p_s^{(0)}}{\sigma^{(0)}} + \frac{w^{(0)}}{\sigma^{(0)}}w_s^{(0)} = 0$$